NUMERICAL ANALYSIS ON COMBUSTION INSIDE RD-108 ROCKET ENGINE

GIRI RAM A/L SREERAMLU

MASTER OF SCIENCE (MECHANICAL ENGINEERING)

UNIVERSITI PERTAHANAN NASIONAL MALAYSIA

2020

NUMERICAL ANALYSIS ON COMBUSTION INSIDE RD-108 ROCKET ENGINE

GIRI RAM A/L SREERAMLU

Thesis submitted to the Centre for Graduate Studies, Universiti Pertahanan Nasional Malaysia, in fulfilment of the requirements for the Degree of Doctor of Philosophy (Civil Engineering)

January 2020

ABSTRACT

Understanding the combustion process that happens in a liquid propellant rocket engine is a challenge, in part because of the turbulent nature of the process. In this study, effort is made to gain more knowledge on the subject by studying the characteristics of combustion inside the rocket nozzle and aspects of performance and efficiency of a rocket. These efforts are made possible by conducting a numerical simulation on RD-108 rocket engine using modern simulation software that allows the study of a wide range of subjects in a short time. The simulation is conducted using Computational Fluid Dynamics technique, specifically 2-Dimensional Navier Stokes equation. Result shows that the most stable and ideal simulation of combustion process in RD-108 rocket nozzle occurs when using the default size of combustion chamber, coarse structural grid, k-ɛ turbulent flow model with re-normalization group, kerosene-air propellants, hybrid initialization and a specific setting to run calculation. A standard model, which contains all of the aforementioned properties is then used to calculate the thrust force and specific impulse. Result shows that while the thrust force deviates from experimental data by over 30%, the specific impulse value has a deviation of 4.46%, verifying the accuracy of the data. Result also shows that the thrust force and specific impulse in hydrogen-air model is more than than kerosene-air model, in agreement with the scientific literature

ABSTRAK

Memahami proses pembakaran yang berlaku dalam mesin roket propelan cecair adalah satu cabaran, kerana sifat proses turbulence yang berlaku di dalamnya. Dalam kajian ini, usaha dilakukan untuk mengatahui secara mendalam mengenai ciri-ciri pembakaran di dalam nozzle roket dan aspek prestasi dan kecekapan roket. Usahausaha ini boleh dilakukan oleh sebab program simulasi berangka yang menggunakan teknologi moden yang memungkinkan pembelajaran pelbagai aspek pembakaran dalam waktu singkat. Simulasi dilakukan menggunakan teknik Computational Fluid Dynamics, khususnya menggunakan Navier Stokes 2-Dimensi. Hasil kajian menunjukkan bahawa simulasi proses pembakaran yang paling stabil dan ideal dalam muncung roket RD-108 berlaku apabila menggunakan ukuran ruang pembakaran kecil, grid struktur kasar, model aliran turbulen k-ɛ dengan kumpulan normalisasi semula, propelan kerosene-oksigen, hibrid inisialisasi dan tetapan khusus untuk menjalankan pengiraan. Model standard, yang mengandungi semua sifat tersebut kemudian digunakan untuk mengira prestasi dan kecekapan roket. Hasil menunjukkan bahawa nilai thrust force menyimpang dari data eksperimen lebih 30%, tetapi nilai specific impulse mempunyai penyimpangan hanya 4.46%, mengesahkan ketepatan data. Hasil kajian juga menunjukkan bahawa nilai thrust force dan specific impulse bagi model hydrogen-oksigen adalah lebih berbanding model keroseneoksigen, mengesahkan ketepatan dengan journal saintifik.

ACKNOWLEDGEMENTS

First and foremost, I would like to show my earnest gratitude towards my supervisor, Ir. Dr. Mohd Rosdzimin bin Abdul Rahman, without whom this thesis project would not be possible. Not only did he provide constant guidance throughout the duration of the project, he was also very supportive, friendly and generous with his time.

I would also like to thank the examiners during proposal phase, Ir. Dr. Abd Rahim Bin Mat Sarip and Dr. Raja Nor Izawati Binti Raja Othman for giving constructive criticism and valuable advice on how to improve the paper. A heartfelt thanks is also directed to Ir. Dr. Mohd Rashdan bin Saad for providing ample guidance on how to write a thesis paper during the Research Methodology subject, my coursemates for their willingness to share information and resources and the entire UPNM Master of Engineering management faculty for providing the necessary resources and updates when needed.

Lastly, I would like to thank my family for allowing me to pursue this course and being very supportive throughout the way.

APPROVAL

The Examination Committee has met on 4th December 2020 to conduct the final examination of Giri Ram A/L Sreeramlu on his degree thesis entitled 'Numerical Analysis on combustion inside RD-108 Rocket Nozzle.

The committee recommends that the student be awarded the Master of Engineering (Mechanical Engineering)

Members of the Examination Committee were as follows.

Ir. Dr. Abd Rahim Bin Mat Sarip

Faculty of Engineering Universiti Pertahanan Nasional Malaysia (Internal Examiner)

Ir. Dr. Mohd Rashdan bin Saad

Faculty of Engineering Universiti Pertahanan Nasional Malaysia (Internal Examiner)

APPROVAL

This thesis was submitted to the Senate of Universiti Pertahanan Nasional Malaysia and has been accepted as fulfilment of the requirements for the degree of **Master of Engineering (Mechanical Engineering)**. The members of the Supervisory Committee were as follows.

Ir. Dr. Mohd Rosdzimin bin Abdul Rahman

Faculty of Engineering Universiti Pertahanan Nasional Malaysia (Supervisor)

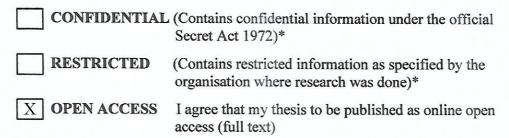
UNIVERSITI PERTAHANAN NASIONAL MALAYSIA

DECLARATION OF THESIS

Student's full name	: GIRI RAM A/L SREERAMLU
Date of birth	: 25/08/1991
Title	: NUMERICAL ANALYSIS ON COMBUSTION INSIDE RD-108 ROCKET ENGINE
Academic session	: 2019/2020

I hereby declare that the work in this thesis is my own except for quotations and summaries which have been duly acknowledged.

I further declare that this thesis is classified as:



I acknowledge that Universiti Pertahanan Nasional Malaysia reserves the right as follows.

- 1. The thesis is the property of Universiti Pertahanan Nasional Malaysia.
- 2. The library of Universiti Pertahanan Nasional Malaysia has the right to make copies for the purpose of research only.
- 3. The library has the right to make copies of the thesis for academic exchange.

Signature

**Signature of Supervisor/Dean of CGS/ Chief Librarian

910825-14-5531

IC/Passport No.

Assoc Prof Ir Dr Mohd Rosdzimin Abdul Rahman **Name of Supervisor/Dean of CGS/

Chief Librarian

Date: 26/10/2020

Date: 26 Oct 2020

Note: *If the thesis is CONFIDENTAL OR RESTRICTED, please attach the letter from the organisation stating the period and reasons for confidentiality and restriction.

** Witness

TABLE OF CONTENTS

		Page
ABSTRACT		ii
ABSTRAK		iii
ACKNOWL	EDGEMENTS	iv
APPROVAL		v
DECLARAT	TION	vii
TABLE OF	CONTENTS	viii
LIST OF TA	ABLES	Х
LIST OF FI	GURES	xi
LIST OF AB	BREVIATIONS	xii
CHAPTER		
1	INTRODUCTION	1
	1.1 Problem Statement	1
	1.2 Background	2
	1.2.1 Overview	
	1.2.2 Rocket Compartments	2 3 3
	1.2.3 Rocket Propulsion Systems	3
	1.2.4 Rocket Propellants	4
	1.2.5 History of RD-108 LPRE	5
	1.2.6 Computational Fluid Dynamics (CFD)	6
	1.2.7 Combustion Characteristics	7
	1.2.8 Performance and Efficiency	8
	1.3 Objectives	9
	1.4 Research Scope	10
	1.5 Research Limitations	10
2	LITERATURE REVIEW	11
	2.1 Geometry of Rocket Nozzle	11
	2.2 Structural Grid	12
	2.3 Governing Equations	14
	2.4 Types of Fuel	16
	2.5 Types of Oxidizers	17
	2.6 Equivalence Ratio	18
	2.7 Types of Injector	19
	2.8 Viscosity of Flow	20
	2.9 Supercritical Conditons	21
	2.10 Combustion Instability	22
	2.11 Rocket Plume	24
	2.12 Performance and Efficiency	25
3	METHODOLOGY/MATERIALS AND METHODS	27
	3.1 Geometry of Rocket Nozzle	27
	3.2 Structural Grid	31

	3.3 Governing Equations	32	
	3.4 Boundary and Initial Conditons	34	
	3.5 Simulation Settings	36	
	3.6 Project Flow Chart	37	
	3.7 Project Gantt Chart	37	
4	RESULTS AND DISCUSSION	38	
	4.1 Validation	38	
	4.1.1 Inviscid Flow	38	
	4.1.2 Standard Model	41	
	4.2 Parametric Geometry	43	
	4.3 Structural Grid	45	
	4.4 Viscosity of Flow	48	
	4.4.1 Laminar Flow	48	
	4.4.2 K-epsilon Turbulent Flow	50	
	4.4.3 K-omega Turbulent Flow	50	
	4.4.4 Despatched Eddy Simulation Turbulent Flow	52	
	4.5 Propellants	53	
	4.5.1 Methane-Air	53	
	4.5.2 Hydrogen-Air	55	
	4.5.3 Freeze and Finite Method	57	
	4.6 Boundary and Initial Conditions	59	
	4.6.1 Parameters	59	
	4.6.2 Standard and Hybrid Initialization	60	
	4.6.3 Courant Number and Iterations	61	
	4.7 Performance	62	
	4.8 Efficiency	63	
5	Conclusion	64	
REFERENCES/BIBLIOGRAPHY			
. –	APPENDICES		
A. Flow Chart		70	

B. Gantt Chart 70

LIST OF TABLES

TABLE NO.	TITLE	PAGE
1	Table 3.1: Boundary and Initial Conditions for the Standard Model	35
2	Table 3.2: Position-specific boundary condition for standard model	35
3	Table 3.3: Boundary & Initial Conditions for the Methane- Air Model	36
4	Table 3.4: Boundary & Initial Conditions for the Hydrogen- Air Model	36

LIST OF FIGURES

TITLE PAGE FIGURE NO. 1 Figure 1.1: Replica of RD-108 LPRE (Wade, 2020) 6 Figure 1.2: The velocity requirement in a convergent-2 divergent nozzle. (mach number: velocity magnitude = 8 1Ma:343m/s) Figure 2.1: Description of various cross-sectional area in a 3 11 rocket nozzle Figure 2.2: Tetrahedral element (left) and hexahedral 4 13 element (right) with nodal points (Ho, 2008) Figure 2.3: Comparison of RD-108 LPRE structural grid with a high percentage of Tetrahedral elements (above) and 5 13 100% Hexahedral elements (below) 6 Figure 2.4: Rocket plume of developed RD-108 LPRE 25 Figure 3.1: RD-108 Rocket nozzle design (in cm)(Lpre.de, 7 28 2020) Figure 3.2: Design of RD-108 nozzle used for simulations, 8 28 also for standard model (in mm) 9 Figure 3.3: Labels for RD-108 design 29 10 Figure 3.4: 3-dimensional RD-108 design 29 Figure 3.5: Design of RD-108 nozzle with outer space (in 11 30 mm) Figure 3.6: Design of RD-108 nozzle with extended 12 30 combustion chamber (in mm) 13 Figure 3.7: Fine grid of design 3.1.2 half-rocket nozzle 31 14 Figure 3.8: Course grid of design 3.1.2 half-rocket nozzle 31 Figure 4.1: Contour of velocity in terms of Mach Number 39 15 for inviscid flow setting. Figure 4.2: Graph of static and total temperature for inviscid 39 16 flow setting Figure 4.3: Graph of static and absolute pressure for inviscid 17 40 flow setting Figure 4.4: Contour of velocity magnitude for standard 18 42 condition Figure 4.5: Contour of static temperature for standard 19 42 condition 20 Figure 4.6: Contour of static pressure for standard condition 43

21	Figure 4.7: Contour of velocity magnitude for extended chamber design	43
22	Figure 4.8: Contour of static temperature for extended chamber design	44
23	Figure 4.9: Contour of static pressure for extended chamber design	44
24	Figure 4.10: Side-to-side comparison of fine grid (above) and coarse grid (below)	46
25	Figure 4.11: Contour of velocity magnitude for fine grid	47
26	Figure 4.12: Contour of static temperature for fine grid	47
27	Figure 4.13: Contour of static pressure for fine grid	48
28	Figure 4.14: Contour of velocity magnitude for laminar flow	49
29	Figure 4.15: Contour of static temperature for laminar flow	49
30	Figure 4.16: Contour of static pressure for laminar flow	50
31	Figure 4.17: Contour of velocity magnitude for k-omega turbulence model	51
32	Figure 4.18: Contour of static temperature for k-omega turbulence model	51
33	Figure 4.19: Contour of static pressure for k-omega turbulence model	51
34	Figure 4.20: Contour of velocity magnitude for DES turbulence model	52
35	Figure 4.21: Contour of static temperature for DES turbulence model	52
36	Figure 4.22: Contour of static pressure for DES turbulence model	53
37	Figure 4.23: Contour of velocity magnitude for methane-air model	54
38	Figure 4.24: Contour of static temperature for methane-air turbulence model	54
39	Figure 4.25: Contour of static pressure for methane-air turbulence model	55
40	Figure 4.26: Contour of velocity magnitude for hydrogen-air model	56
41	Figure 4.27: Contour of static temperature for hydrogen-air model	56
42	Figure 4.28: Contour of static pressure for hydrogen-air model	57
43	Figure 4.29: Contour of velocity magnitude for freeze model	58
44	Figure 4.30: Contour of velocity magnitude for freeze model	58

45	Figure 4.31: Contour of velocity magnitude for freeze model	59
46	Figure 4.32: Contour of velocity magnitude for half-nozzle at velocity-inlet setting of 200m/s (above) and 50m/s (below).	60
47	Figure 4.33: Graph of thrust force vs model type	62
48	Figure 4.34: Graph of specific impulse vs model type	63

LIST OF ABBREVIATIONS

UPNM	Universiti Pertahanan Nasional Malaysia
MINDEF	Ministry of Defence
STRIDE	Science and Technology Research Institute for Defence
CFD	Computational Fluid Dynamics
LPRE	Liquid Propellant Rocket Engine
RANS	Reynolds Average Navier-Stokes
LES	Large Eddy Simulation
DES	Detached Eddy Simulation
RNG	Renormalization Group Theory

CHAPTER 1

INTRODUCTION

1.1 Problem Statement

Liquid propellant rocket engines (LPRE) have been studied extensively for well over a century. Numerical modelling and simulation of rocket engines using Computational Fluid Dynamics (CFD) calculations have been studied since the 1940s. With the introduction of computer-aided software, the time taken to process the calculations and number of iterations have become a lot shorter.

However, to the knowledge of the author, few studies have conducted the numerical simulation of rocket nozzle with a modern simulation software that is capable of studying a wide range of combustion characteristics in a short span of time. Most studies focused on one or two characteristics in detail, and one of the reasons could be due to software limitations.

Even fewer studies focused on the combustion characteristics of RD-108 rocket nozzle. This could be in part because it is an old design. Although old, it was found through this study a lot can be learned about the nature of combustion from the numerical simulation of this design of nozzle. It was also found through this study

that the benefit of simulating old designs is that there is adequate experimental data to compare simulated data with for accuracy of computation.

Therefore, efforts were made to study the combustion characteristics, performance and efficiency of RD-108 rocket engine.

1.2 Background

1.2.1 Overview

Rocket science and technology have gained tremendous popularity in recent years. This is because of private companies such as SpaceX, Blue Origin and Virgin Galactic, that aim to commercialize space travel in the future, promising to create new industries such as space tourism. As a result, the rate of technological development in this field has accelerated.

For a long time since the Cold War era, the space industry experienced a lack of progress. This is because of the lack of investment and government-funding. Therefore, the recent developments are a positive sign for the industry. If an industry like space tourism is created and thrives, then there is possibility for many countries, including those that are underdeveloped in rocket science and technology, to benefit.

Other than human spaceflights, space exploration has been and still is a major factor in rocket technology development. In the past, the race to land the first human on the moon drove United States of America and the Soviet Union to improve their rocket technology. In the present, there is a competition to land the first human on planet Mars and it has garnered interest. Besides human spaceflight and space exploration, rockets are also used for the purpose of military and launching of satellites.

1.2.2 Rocket Compartments

Rockets can be compartmentalized into four systems, namely the payload, structural, guidance and propellant systems (Andersson, 2019). Payload concerns whatever that is needed to be transported to space, be it astronauts, satellites, missiles, or research materials; the structural system concerns the design and manufacture of various parts of the rocket; the guidance system includes the various communication equipment like radars and sensors that guide rockets in the desired direction; and lastly, the propulsion system includes technologies that enable the rocket to be thrusted from ground to space.

1.2.3 Rocket Propulsion Systems

Rocket propellant engines can be further subdivided into chemical and electric propulsion systems. Electrothermal, electrostatic and electromagnetic propulsion are examples of electric propulsion while liquid, solid and hybrid propulsion are examples of chemical propulsion. Of all the propellant types, by far the most commonly used type for the longest time has been the liquid propellant engine. The main reason for that is because the liquid propellant engine has notable advantages over the other systems. In comparison, electric propulsion systems provide thrust that is relatively small and inefficient, because the power comes from either battery or solar panels. Meanwhile the solid propulsion system is costly and could not be tested first because of its inability to be reusable. The premixed propellant is also potentially explosive should ignition happen unintentionally.

Hybrid propulsion systems are relatively new and so more research and development are needed, particularly research on switching between liquid and solid propulsion. In some cases, solid propellant boosters are used to assist liquid propellant rocket engines in providing additional thrust during lift-off.

1.2.4 Rocket Propellants

There are monopropellant and bipropellant Liquid Propellant Rocket Engine (LPRE), whereby the former uses a single chemical as a propellant while the latter uses two, namely a fuel and an oxidizer. Comparatively, the monopropellant system has a less complex design because of the single tank, but is relatively inefficient and has low thrust, because of the usage of a catalyst to aid the combustion process.

A further subdivision can be made of bipropellant LPRE, into the thrust chamber, propellant feed, liquid and oxidizer tanks and automatic regulators (Wang, 2016). The propellant feed system channels the propellants from the propellant tanks to the injectors in the combustion chamber. Either high pressure in the tank or a turbo pump could be used to push the propellants into the combustion chamber. The thrust chamber is where the chemical propellants are converted to mechanical energy to propel the LPRE forwards. It is made up of combustion chamber and nozzle. Propellants would be injected into the combustion chamber and combustion process would occur. The resulting gases would be channelled by the nozzle backwards and outwards and the flow of various gas species in a very high mass flow rate and at supersonic speeds is what provides thrust force for the rocket to move upwards.

The convergent-divergent shape of the nozzle is necessary to enable this process of turning thermal to kinetic energy to occur. Aside from combustion and compressible gas flow, cooling also takes place inside the thrust chamber; its purpose is to ensure that the internal walls of the thrust chamber do not melt from the high temperature generated during combustion that is higher than the critical temperature of the material of the wall. Some examples of cooling are regenerative cooling and radioactive cooling.

1.2.5 History of RD-108 LPRE

RD-108 LPRE, which was developed by the Soviet Union, has four thrust chambers, uses a kerosene variant called RG-1 as fuel and liquid oxygen as oxidizer (Halchak, 2016).



Figure 1.1: Replica of RD-108 LPRE (Wade, 2020)

1.2.6 Computational Fluid Dynamics (CFD)

Numerical simulation is a calculation that is done using mathematical models to a point where the actual event could be simulated. Since the advent of computers, programs in software run the calculation and simulate a predictive outcome of the studied activity.

In the case of numerical simulation of LPRE, three key processes are necessary, namely the combustion process modelling, numerical model solution and simulation results analysis (Wang, 2016). The first process typically includes heat transfer models, combustion models and atomization models. If turbulence is considered then flow turbulence model is included. The second process works on solving using the mathematical models mentioned previously and the addition of boundary, initial and periodic conditions. CFD used in various software like Ansys and Autodesk CFD work on this process. For the third process, various visualization methods aid in examining in detail the characteristic of the combustion process and performance of the engine.

Among the various benefits of conducting numerical modelling and simulation are that the duration of the developmental stage could be drastically shortened, the cost of research could be greatly reduced and depending on the 7 accuracy of the simulation, problems that would otherwise be glossed over could be detected very early and the experimental process could be conducted with more certainty because of the validation provided by numerical simulation.

1.2.7 Combustion Characteristics

Combustion characteristic is defined to be the features of combustion or the specific details of combustion. It is related to the mechanism of combustion, which means the natural processes that take place during combustion.

In this study, the combustion characteristics of RD-108 LPRE include details as to whether there is change to parameters such as velocity, temperature, pressure, mass flow rate in various parts of the rocket nozzle when there is change to geometry of structure, grid of structure, viscosity of flow, types of fuel, simulation methods, boundary conditions and initial conditions.

Based on the observed patterns of simulation result, analysis was also done on combustion stability or instability, for example whether or not there is a shock wave, is there an under-expansion or over-expansion of flame and which part of the nozzle experiences divergence in calculated value.

Certain criteria need to be met in order for a rocket engine to function. The first is, in a convergent-divergent nozzle design, the velocity needs to be subsonic (less than 343m/s) before the nozzle throat, sonic (equals to 343m/s) at throat and supersonic after nozzle throat, as illustrated in Figure 1.2. Second criteria is, the temperature in the combustion chamber needs to be as high as 3500K. Inability to meet either of these criteria could mean that the combustion process is not conducive for rocket propulsion.

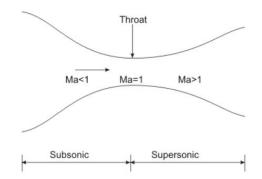


Figure 1.2: The velocity requirement in a convergent-divergent nozzle. (mach number: velocity magnitude = 1 Ma : 343m/s)

1.2.8 Performance and Efficiency

Performance refers to how powerful a certain LPRE is in comparison to other rocket engines. In recent times, due to the focus on cleaner and greener technology, it may also be appropriate to discuss about the role of sustainability and low-emission in the context of LPRE performance. However, for this study only the thrust force of LPRE is used as barometer for performance.

Contrary to popular belief, a high-thrust force is not necessarily desired, this is evidenced by studies such as Chandler (2019) where a low-thrust rocket engine was developed. The reason is because a high thrust rocket engine may not be energy-efficient and could be costly. The idea behind a low-thrust engine is to develop a rocket engine with optimal thrust that is able to escape the velocity barrier of atmosphere but is also efficient and affordable.

Efficiency discusses about how much of the chemical energy from the propellants is converted to thermal energy in the combustion chamber and then kinetic energy that provides thrust to the LPRE. Specific impulse measures how efficiently a certain rocket engine uses propellants.

For this study, the goal is not to improve the RD-108 LPRE performance and efficiency, but to compare the numerically simulated result with available experimental data.

1.3 Objectives

This study embarks on the following objectives:

1. To study the combustion characteristic inside the RD-108 combustion chamber rocket nozzle.

2. To study the performance and efficiency of the liquid propellant rocket engine.

1.4 Research Scope

The scope of research is as follows:

1. The rocket engine is considered to operate in steady state, single-stage and adiabatic condition.

2. The thrust force and specific impulse of numerical simulation needs to tally with reference data with a low margin of error.

3. The velocity at the nozzle needs to be subsonic (Mach number < 1) in the convergence section, sonic at the nozzle throat (Mach number = 1) and supersonic at the divergence section (Mach number > 1).

1.5 Research Limitations

This study is impacted by the following limitations:

1. Low computing power of processor limits the extent to which numerical simulation could be performed in software with Computational Fluid Dynamics program.

2. Due to the short duration of Masters' Thesis project, the numerical study could not be verified by in-house experimental study. However, the reference data was found to be sufficient enough to verify the data from numerical study.